

CrossMark

Available online at www.sciencedirect.com



Procedia Structural Integrity 59 (2024) 575-582

Structural Integrity
Procedia

www.elsevier.com/locate/procedia

# VII International Conference "In-service Damage of Materials: Diagnostics and Prediction" (DMDP 2023)

# Deformability of reinforced concrete beams under the action of repeated alternating loads

Oleksandr Korniychuck<sup>a</sup>, Grigoriy Masiuk<sup>a</sup>, Sviatoslav Homon<sup>a\*</sup>, Ivan Aleksiievets<sup>a</sup>, Oleksandr Chapiuk<sup>b</sup>, Diana Kaynts<sup>c</sup>, Vasyl Rizak<sup>c</sup>

<sup>a</sup>National University of Water and Environmental Engineering, Soborna 11, 33000 Rivne, Ukraine <sup>b</sup>Lutsk National Technical University, Lvivska 75, 43018 Lutsk, Ukraine, <sup>c</sup>Uzhhorod National University, 14 University Str., 88000 Uzhgorod, Ukraine

# Abstract

A technique has been developed, and experimental studies of reinforced concrete beams under repeated alternating loads at different shear spans have been carried out. It has been established that the shear span significantly affects the deformation behaviour in the oblique and normal sections. It was found that with smaller shear spans, the deformations of transverse reinforcement and concrete in oblique sections develop much more intensively and have greater values for the deformation of longitudinal reinforcement and concrete in normal sections. The residual strain appears in the first cycles of overload and decays uniformly in subsequent cycles due to decreased plastic deformations in materials.

© 2024 The Authors. Published by Elsevier B.V. This is an open access article under the CC BY-NC-ND license (https://creativecommons.org/licenses/by-nc-nd/4.0) Peer-review under responsibility of DMDP 2023 Organizers

Keywords: repeated alternating loads, reinforced concrete beam, reinforcement, deformability, bending.

\* Corresponding author. Tel.: +380962020907. *E-mail address:* homonsviatoslav@ukr.net

2452-3216 © 2024 The Authors. Published by ELSEVIER B.V. This is an open access article under the CC BY-NC-ND license (https://creativecommons.org/licenses/by-nc-nd/4.0) Peer-review under responsibility of DMDP 2023 Organizers 10.1016/j.prostr.2024.04.081

#### 1. Introduction

At the present stage of construction development, materials, products, elements and structures based on wood (Gomon et al. (2022); Yasniy et al. (2022); Homon et al. (2023); Janiak et al. (2023); Pavluk et al. (2023)), metal (Kovalchuk (2018), Iasnii et al. (2023); Imbirovych et al. (2023); Prentkovskis et al. (2023)), concrete (Dvorkin et al. (2021), Protsiuk et al. (2023); Iskhakov et al. (2022); Konkol (2019)) and reinforced concrete (Babych et al. (2019); Kos et al. (2022), Mel'nyk (2019); Iskhakov et al. (2023)), as well as various composites are often used (Mikulich (2023); Shvabyuk et al. (2017)). The most common are bending elements (Romashko and Romashko-Maistruk (2023); Gomon et al. (2023); Sobczak- Piastka et al. (2020); (Gomon et al. (2022)). In the construction of industrial, public, residential buildings and engineering structures (Bosak et al. (2011)) reinforced concrete elements and structures are very often used as load-bearing structures (Masiuk et al. (2018); Kos et al. (2022); Babych et al. (2019); Mel'nyk (2019)).

Nomenclature	
E <sub>c</sub>	relative deformations of concrete in normal sections
E <sub>s</sub> E <sub>cw</sub>	relative deformations of concrete in oblique sections
$\mathcal{E}_{sw}$	relative deformations of transverse reinforcement shear span
h	beam hight
l <sub>0</sub> n	beam span number of loading cycles
F	concentrated force
$F_u$ $\eta$	loading level

In modern design of reinforced concrete structures the calculation is carried out according to limit states using coefficients of operating conditions (DBNB.1.2-14-2018 (2018); DSTUBV.2.6-156:2010 (2011); EN 1992-1-1 (2004)). They establish a systematic dependence of the materials properties on loads but do not consider the influence of the loading history and its nature on the change in the destructive, strength and deformation characteristics of concrete and reinforcement.

A large number of reinforced concrete structures during operation are subjected to low-cycle repeated and alternating loads (Masiuk et al. (2018)), which can occur within the operational level or exceed it. Such loads include wind, technological, seismic, temperature and humidity, and other ones (Famulyak et al. (2019), Borysiuk et al. (2019); Shvabyuk et al. (2014)). Alternating loads and deformations occur in continuous beams, edge columns of industrial buildings, load-bearing and prestressed structures, etc.

The current calculation standards (DBNB.1.2-14-2018 (2018); DSTUBV.2.6-156:2010 (2011); EN 1992-1-1, (2004)) do not take into account the effect of such loads on the change in the physical and mechanical properties of concrete and stress-strain state, since this issue has not been studied enough.

So, the research goal is to conduct experimental studies and analyze the deformation characteristics of concrete, transverse and longitudinal reinforcement in bending reinforced concrete elements at various shear spans and loading levels.

# 2. Methodology of experimental studies

The research object is the reinforced concrete beams of rectangular sections with nominal dimensions of 100x160x2000 mm of heavy concrete of C25/30 natural hardening class. The beams are reinforced with two flat welded frames united into a spatial one (see Fig.1a). Longitudinal reinforcement is adopted with a diameter of 14 mm and of A500C class (reinforcement - double, symmetrical), which is securely anchored along the edges of the

beams from sliding in the body of concrete. The transverse reinforcement is made of clamps with a diameter of 4 mm of the Vr-I class with a step of 75 mm on the support sections.

Testing was carried out on equipment that allows the creation of alternating loads on the beams without changing their position (see Fig.1b,c). The beams were tested with a static load - two concentrated forces F, symmetrically mounted relative to the middle of the span, as single-span hinged beams with an estimated span of 1800 mm. In the process of experimental studies of reinforced concrete beams, the relative shear span *a* was changed and taken as  $a = 300 \text{ mm} (a/h \approx 2)$ ,  $a=450 \text{ mm} (a/h \approx 3)$ ,  $a=600 \text{ mm} (a/h \approx 4)$ .

The design of samples and loading schemes are shown in Fig.1a,b,c.



Fig. 1. Design of samples (a), loading schemes (b) and the installation scheme (c): 1 – installation frame; 2 - jack; 3 – dynamometer; 4 - traverse; 5 - supports; 6 - sample; 7 - tips; 8 - pumping station.

Deformations of concrete in calculated sections and deformations of longitudinal and transverse reinforcement were measured by mechanical and tensometric instruments (see Fig.2)



Fig. 2. Layout of measuring devices: I – dial indicator 2MIG; T – Hugenberger strain gauge; TSA - strain gauges with a base of 20 mm (installed on the reinforcement); TSC – a strain gauge with a base of 50 mm (installed on concrete); P is a deflection gauge 6PAO.

The beams were tested with a ten-cycle alternating load (in half-cycles "a" and "b" with the first half-cycle of tension in the lower zone). The beams were loaded in steps with a holding time of 10 minutes at each "loading-unloading" half-cycle.

Beams B4-3/0.65, B4-4.5/0.65 and B4-6/0.65 were loaded in half-cycles up to the level of  $\eta$ =0.65 Fu from the destructive load, which corresponds to the calculated operational value of loads on structures. On the fifth cycle, the samples were additionally loaded to  $\eta$ =0.8 Fu, which corresponds to the calculated limit load. After ten "loading-unloading" cycles, the beams were fractured on the "10-b" half-cycle without unloading. A total of 3 beams were tested.

#### 3. Research results and discussion

Based on the conducted experimental studies, it was established that the stress-strain state of the calculated crosssections of the tested beams depends on the load level and the shear span.

With a decrease in the shear span, the deformations of the transverse reinforcement and concrete in the areas of oblique sections increase at the same level of loading, as evidenced by the " $\epsilon$ -n" graphs (see Fig.3a,b,c and Fig.4a,b,c).



Fig. 3. Graphs of transverse reinforcement deformations by cycles in beams with different shear spans: B4-6 / 0.65 (a), B4-4.5 / 0.65 (b), B4-3 / 0.65 (c).

It should be noted that the deformations of the transverse reinforcement, regardless of the shear span, have a similar character: in the "b" half-cycle, the deformations are always greater than the corresponding deformations in the "a" half-cycle. However, the largest increase in the deformations of the transverse reinforcement with a change in the alternating load is observed at a shear span of a = 450 mm (B4-4.5 / 0.65 beam), namely, by 3.9 times in the first cycle. At the same time, for the shear span of a = 300 mm (B4-3/0.65 beam) in the half-cycle "b" the deformations of the transverse reinforcement increased by 2 times, and of a = 600 mm (B4-6/0.65 beam) - by 1.25 times. An increase in the deformation of the transverse reinforcement when the value of the load applied changes (in the half-cycle "b"), can be explained by the destructive processes occurring in the oblique: the concrete is

decompacting, the grafting with the reinforcement is lost, and as a result, most of the transverse force is perceived by the clamps, and not by the concrete.

As can be seen from the graphs (see Fig.4a,b,c), the change in the shear span affects the nature of the concrete deformation in the oblique sections of the experimental beams. In beams with a shear span of a = 600 mm, the total tensile strains of concrete in the "b" half-cycle is 2.4 times greater than the deformations in the "a" half-cycle (see Fig.4a). For shear spans of 450 and 300 mm, on the contrary, on the half-cycle "a" is greater than the deformation in the half-cycle "b" by 2.1 and 1.1 times, respectively (see Fig.4b,c).



Fig. 4. Graphs of concrete deformations in oblique sections by cycles in beams with different shear spans: B4-6/0,65 (a), B4-4,5/0,65 (b), B4-3/0,65 (c).

The longitudinal reinforcement and concrete deformations in normal sections of the experimental beams are shown in Fig.5a,b,c and Fig.6a,b,c. A change in the shear span also affects the nature of the deformation of both longitudinal reinforcement and concrete.

Longitudinal reinforcement deformations in "b" half-cycles with a shear span of a = 600 mm are 1.03...1.2 times greater than similar deformations in "a" half-cycles. A similar pattern of deformations is also observed for a span of 450 mm. As for the deformations of the longitudinal reinforcement in the beams with a shear span of 300 mm, they are almost the same in the half-cycles "a" and "b".

Deformations of concrete in normal sections of experimental beams with spans of a = 600 and 450 mm in half-cycles "b" are 1.5 ... 2.0 times greater than similar deformations in half-cycles "a". Concrete deformations are almost the same in beams with a shear span of 300 mm. This fact can be explained by a rather small shear span ( $a/h \approx 2$ )



and, therefore, insignificant influence of the alternating load on the operation of normal sections (both for reinforcement and concrete).

Fig. 5. Graphs of longitudinal reinforcement deformations by cycles in beams with different shear spans: B4-6/0,65 (a), B4-4,5/0,65 (b), B4-3/0,65 (c).



Fig. 6. Graphs of concrete deformations in normal sections by cycles in beams with different shear spans: B4-6/0,65 (a), B4-4,5/0,65 (b), B4-3/0,65 (c).

### 4. Conclusions

The following conclusions can be drawn from the article: 1) a methodology has been developed, and experimental studies of reinforced concrete beams under the action of repeated alternating loads at various shear spans have been carried out; 2) the shear span has a significant effect on the nature of the deformation of the materials in oblique and normal sections; 3) with smaller shear spans the deformations of transverse reinforcement and concrete in oblique sections develop much more intensively and have greater values than the deformation of longitudinal reinforcement and concrete in normal sections; 4) residual deformations appear in the first cycles of loading and gradually fade in subsequent cycles due to a decrease in plastic deformations in materials; 5) these experimental studies can be used by designers in the calculation of bending reinforced concrete elements under the action of repeated alternating loads.

#### References

- Babych, Y., Filipchuk, S., Fenko, O., 2018. Mathematical modeling of the resistance of pulling out steel bars from high strength concrete. International Journal of Engineering and Technology 7 (3.2), 516-521.
- Babych, Y.M., Savitskiy, V.V., Andriichuk, O.V., Ninichuk, M.V., Kysliuk, D.Y., 2019. Results of experimental research of deformability and crack-resistance of two span continuous reinforced concrete beams with combined reinforcement. IOP Conference Series: Materials Science and Engineering 708(1), 012043.

Borysiuk, O., Karavan, V., Sobczak-Piastka, J., 2019. Calculation of the normal section strength, rigidity and crack resistance of beams,

strengthened by carbon-fiber materials. AIP Conference Proceedings 2077, 020008.

- Bosak, A., Matushkin, D., Dubovyk, V., Homon, S., Kulakovskyi, L., 2021. Determination of the concepts of building a solar power forecasting model. Scientific Horizons 24(10), 9-16.
- DBN B.1.2-14-2018, 2018. Zahalni pryntsypy zabezpechennia nadiinosti ta konstruktyvnoi bezpeky budivel i sporud [General principles of ensuring the reliability and structural safety of buildings and structures]. Ministry of Regional Development of Ukraine, Kyiv, pp. 30.
- DSTU B V.2.6-156:2010, 2011. Betonni ta zalizobetonni konstruktsii z vazhkoho betonu. Pravyla proektuvannia [Concrete and reinforced concrete structures made of heavy concrete. Design rules]. Ministry of Regional Development of Ukraine, Kyiv, pp. 123. EN 1992-1-1, 2004.
- Dvorkin, L., Bordiuzhenko, O., Zhitkovsky, V., Gomon, S., Homon, S., 2021. Mechanical properties and design of concrete with hybrid steel basalt fiber. E3S Web of Conferences 264, 02030.
- EN 1992-1-1, 2004.Eurocode 2: Design of Concrete Structures Part 1-1: General rules and rules for buildings. CEN, Brussels, pp. 225.
- Famulyak, Y., Hrytsevych, A., Sobczak-Piastka, J., 2019. Influence of Freeze-Thaw Temperature on Load-Bearing Capacity of Steel-Concrete Beams Carrying Transverse Loads. IOP Conference Series: Earth and Environmental Science 362(1), 012115.
- Gomon, P., Gomon, S., Pavluk, A., Homon, S., Chapiuk, O., Melnyk, Yu., 2023. Innovative method for calculating deflections of wooden beams based on the moment-curvature graph. Procedia Structural Integrity 48, 195-200.
- Gomon, S.S., Gomon, P., Homon, S., Polishchuk, M., Dovbenko, T., Kulakovskyi, L., 2022. Improving the strength of bending elements of glued wood. Procedia Structural Integrity 36, 217-222.
- Gomon, S., Gomon, P., Korniychuck, O., Homon, S., Dovbenko, T., Kulakovskyi, L., Boyarska, I., 2022. Fundamentals of calculation of elements from solid and glued timber with repeated oblique transverse bending, taking into account the criterion of deformation. Acta Facultatis Xylologiae Zvolen 64(2), 37-47.
- Homon, S., Gomon, P., Gomon, S., Vereshko, O., Boyarska, I., Uzhegova, O., 2023. Study of change strength and deformation properties of wood under the action of active acid environment. Proceedia Structural Integrity 48, 201-206.
- Homon, S., Litnitskyi, S., Gomon, P., Kulakovskyi, L., Kutsyna, I., 2023. Methods for determining the critical deformations of wood at various moisture. Scientific Horizons 26(1), 73-86.
- Iasnii, V., Yasniy, O., Homon, S., Budz, V., Yasniy, P., 2023. Capabilities of self-centering damping device based on pseudoelastic NiTi wires. Engineering Structures 278, 115556.
- Imbirovych, N., Boyarska, I., Povstyanoy, O., Kurdzydlowski, K., Homon, S., Kulakovskyi, L., 2023. Modification of oxide coatings synthesized on zirconium alloy by the method of plasma electrolytic oxidation. AIP Conference Proceedings 2949, 020011.
- Iskhakov, I., Frolov, I., Ribakov, Y., 2022. Experimental verification of theoretical stress-strain model for compressed concrete considering postpeak stage. Materials 15(17), 6064
- Iskhakov, I., Ribakov, Y., Holschemacher, K., Kaeseberg, S., 2023. Elastic-plastic stage of transverse deformations in the compressed zone of real reinforced concrete beams. Applied Sciences (Switzerland) 13(4), 2306.
- Janiak, T., Homon, S., Karavan, V., Gomon, P., Gomon, S.S., Kulakovskyi, L., Famulyak, Y., 2023. Mechanical properties of solid deciduous species wood at different moisture content. AIP Conference Proceedings 2949, 020009.
- Konkol, J. Fracture toughness and fracture surface morphology of concretes modified with selected additives of pozzolanic properties. Buildings, 2019, 9(8), 174.
- Kos, Z., Klymenko, Y., Karpiuk, I., Grynyova, I., 2022. Bearing capacity near support areas of continuous reinforced concrete beams and high grillages. Applied Sciences (Switzerland) 12(2), 685.
- Kovalchuk, V., Kovalchuk, Y., Sysyn, M., Stankevych, V., Petrenko, O., 2018. Estimation of carrying capacity of metallic corrugated structures of the type Multiplate MP 150 during interaction with backfill soil. Eastern-European Journal of Enterprise Technologies 1(1-91), 18–26.
- Masiuk, G., Yushchuk, O., Paschenko, A., 2018. Experimental investigations of the stress and strain state of continuous reinforced concrete beams under the action of low-cyclic repetitive and alternating loads. International Journal of Engineering & Technology 7 (3.2), 236-238.
- Mel'nyk I., 2019. Stiffness of monolithic reinforced-concrete slab structures. Materials Science 55(3), 367-373.
- Mikulich, O., 2023. Dispersion properties of waves in polyurethane foam. Lecture Notes in Mechanical Engineering, 230-236.
- Pavluk, A., Gomon, S., Ziatiuk Y., Gomon, P., Homon, S., Kulakovskyi, L., Iasnii, V., Yasniy, O., Imbirovych, N., 2023. Stiiffness of solid wood beams under direct and oblique bending conditions. Acta Facultatis Xylologiae Zvolen 65(2), 109-121.
- Prentkovskis, O., Maruschak, P., Panin, S., Berto, F., 2023. Application of alloys in transport. Metals 13(1), 31.
- Protsiuk, V., Andriichuk, O., Shymchuk, O., Ninichuk, M., 2023. Prerequisites for the application of dispersed reinforced concrete for road construction in European countries and USA. AIP Conference Proceedings 2684, 030036
- Romashko, V., Romashko-Maistruk, O., 2023. Regularities of level formation of normal cracks in stretched reinforced concrete elements. AIP Conference Proceedings 2684, 030038.
- Shvabyuk, V.I., Mikulich, O.A., Shvabyuk, V.V., 2017. Stress State of Foam Media with Tunnel Openings Under Non-Stationary Dynamic Loading. Strength of Materials 49(6), pp. 818–828.
- Shvabyuk, V., Rotko, S., Uzhegova, O. 2014. Bending of a composite beam with a longitudinal section. Strength of Materials 46(4), 558-566.
- Sobczak-Piastka, J., Babych, Y, Filipchuk, S, Karavan, V., Nalepa, O., 2020. Research of deformative properties of concrete taking into account the descending branch of deformation. IOP Conference Series: Materials Science and Engineering 960(3), 032057.
- Sobczak-Piastka, J., Gomon, S.S., Polishchuk, M., Homon, S., Gomon, P., Karavan, V., 2020. Deformability of glued laminated beams with combined reinforcement. Buildings 10(5), 92.
- Sobczak-Piastka, J., Pavluk A., Gomon, S.S., Gomon, P., Homon, S., Lynnyk, I., 2023. Changing the position of the neutral line of beams made of glued wood in conditions of oblique bending. AIP Conference Proceedings 2928, 080007.
- Yasniy, P., Homon, S., Iasnii, V, Gomon, S.S., Gomon, P., Savitskiy, V., 2022. Strength properties of chemically modified solid woods. Procedia Structural Integrity 36, 211-216.